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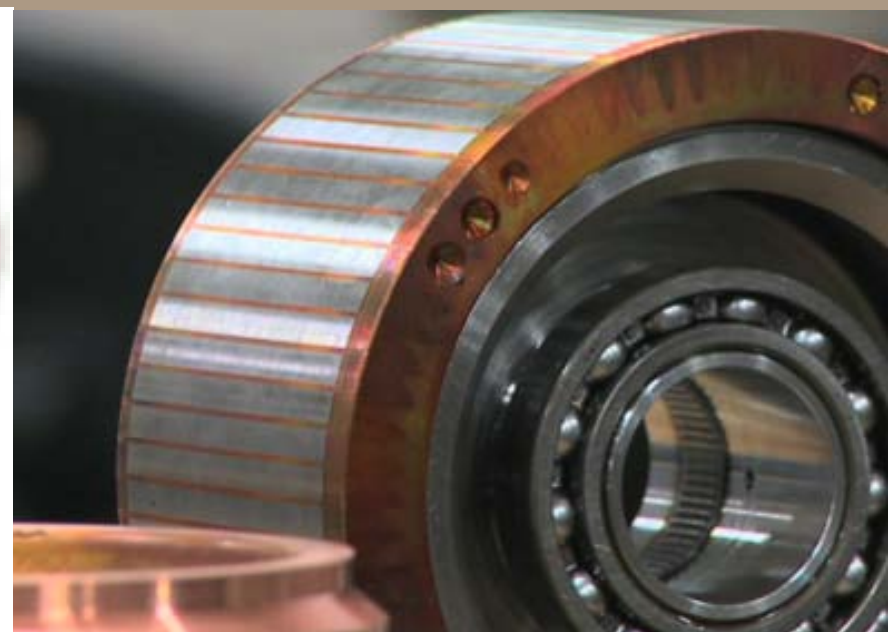


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Performance/cost comparison of induction-motor & permanent-magnet-motor in a hybrid electric car

Malcolm Burwell – International Copper Association
James Goss, Mircea Popescu - Motor Design Ltd

July 2013 - Tokyo

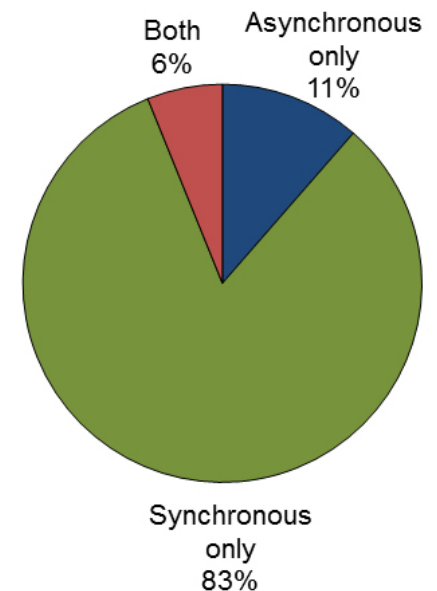


Is it time for change in the traction motor supply industry?

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*“[Our] survey of 123 manufacturers shows far too few making asynchronous or switched reluctance synchronous motors... **this is an industry structured for the past that is going to have a very nasty surprise when the future comes.**” **

Motor-types sold by suppliers of vehicle traction motors *

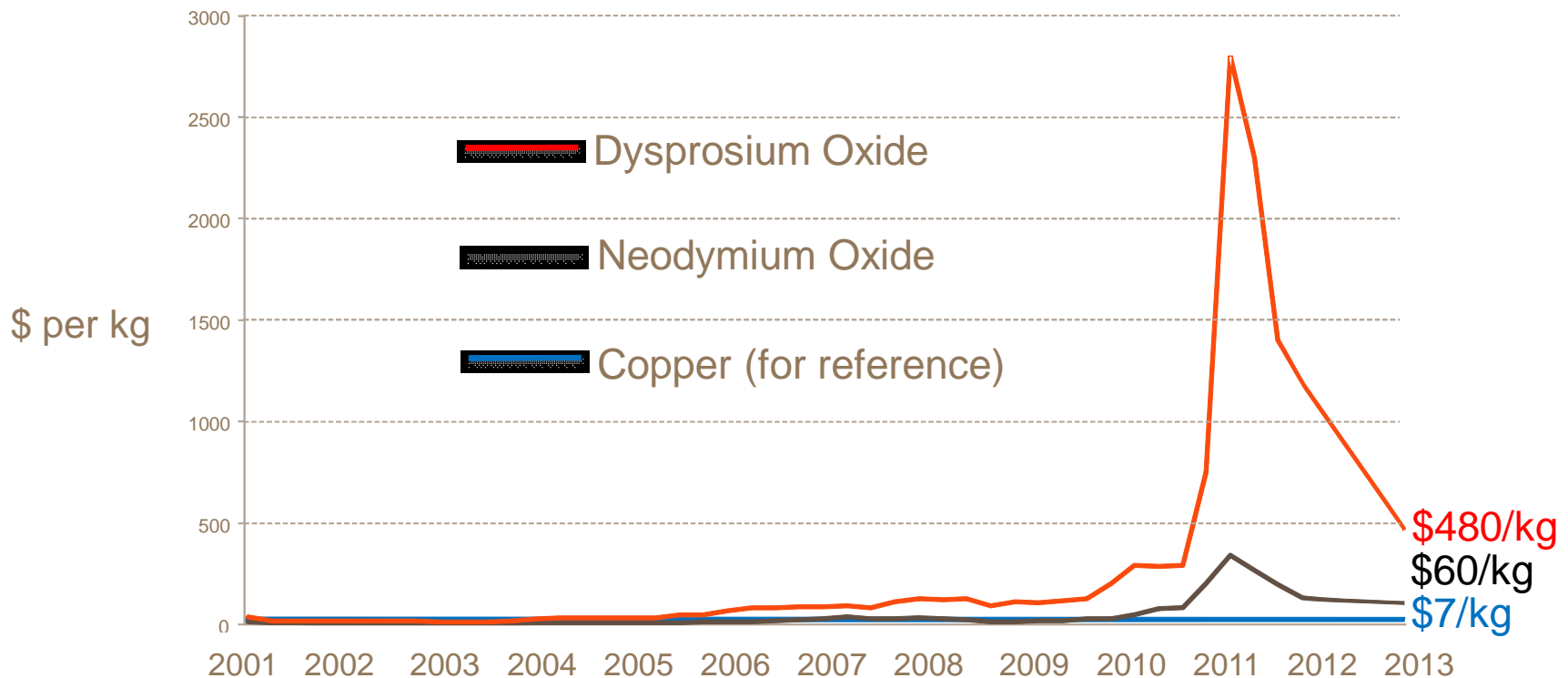


* Source: IDTechEx research report “Electric Motors for Electric Vehicles 2013-2023: Forecasts, Technologies, Players”

www.IDTechEx.com/emotors

The challenge for electric traction motors: rare earth cost-levels and cost-volatility

Cu



Source: metal-pages.com, Kidela Capital

Today, the permanent magnet motor is the leading choice for traction drives in hybrid vehicles

But permanent magnet motors have challenges:

- High costs
- Volatile costs
- Uncertain long term availability of rare earth permanent magnets

This makes alternative magnet-free motor architectures of great interest

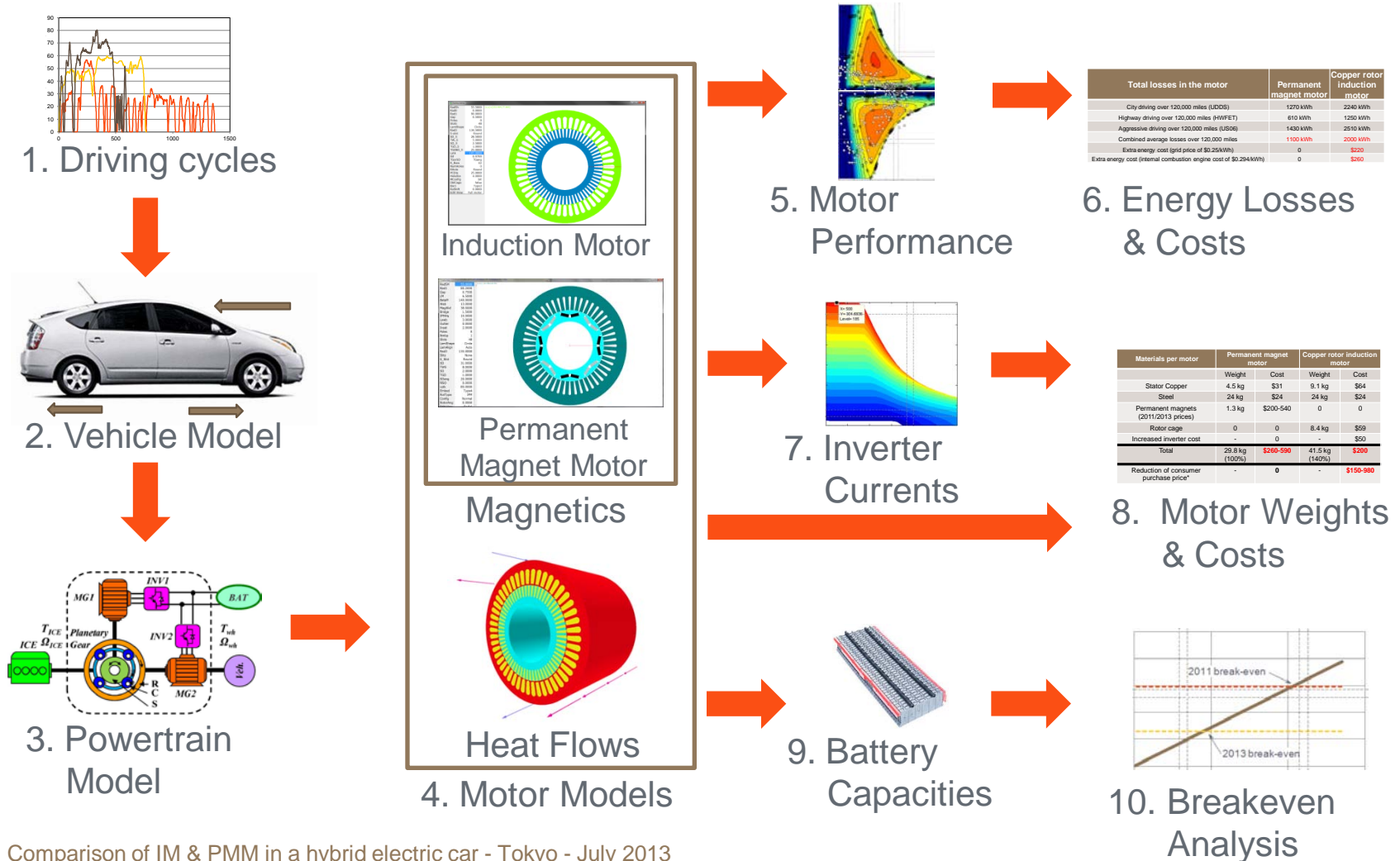
The induction motor is one such magnet-free architecture

The work presented here compares two equivalent 50kW tractions motors for use in hybrid electric vehicles: a permanent magnet motor and an equivalent induction motor

- The main analysis has copper as the rotor cage material of an induction motor
- Motoring and generating modes are modelled using standard drive cycles
- Important outputs of the work, for each motor type, are:
 - Lifetime energy losses and costs
 - Relative component performance parameters, weights and costs
- Top-level comments on aluminium cages are presented at the end

Overview of the analysis covered in this presentation

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Main conclusions from this work

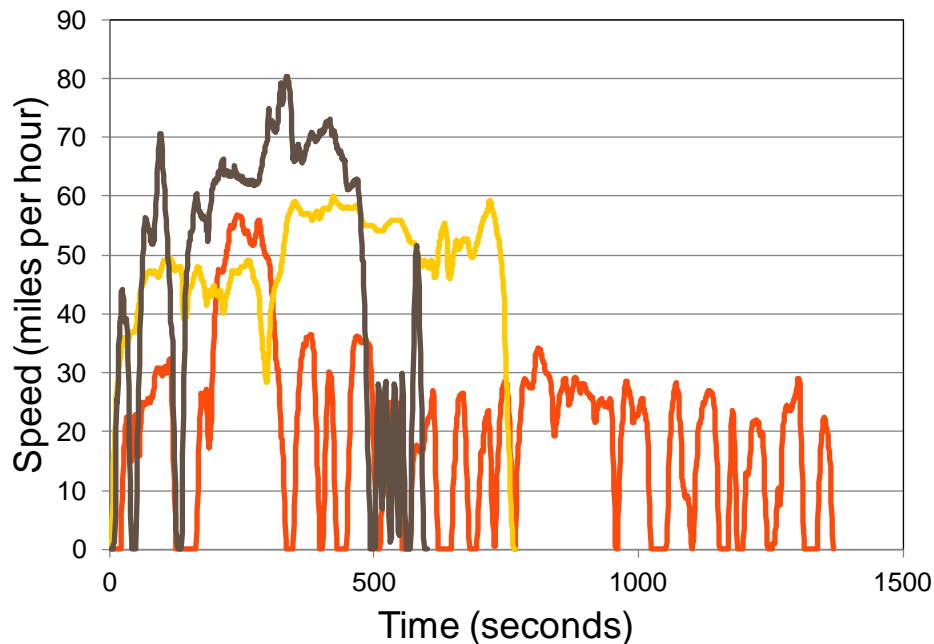
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- Comparing a 50kW copper-rotor induction motor to a 50kW permanent magnet motor:
 - No rare earth metals used
 - -25% torque density
 - +40% weight
 - +10-15% peak inverter current
- However, the induction motor is a good alternative because:
 - Total motor+inverter unit costs are \$60-\$390 less (=\$150-980 lower sticker price)
 - It uses only \$260 in extra energy over 120,000 miles
 - Increased inverter costs are modest at ~\$50/vehicle
- Battery size:
 - Can optionally be increased to match increased motor losses
 - Unit cost savings are larger than increased battery costs up to 27kWh battery size
- Using aluminum instead of copper in the rotor of a 50kW induction motor for an HEV:
 - Increases losses by 4%
 - Lowers torque density by 5%

1. Vehicle drive cycles

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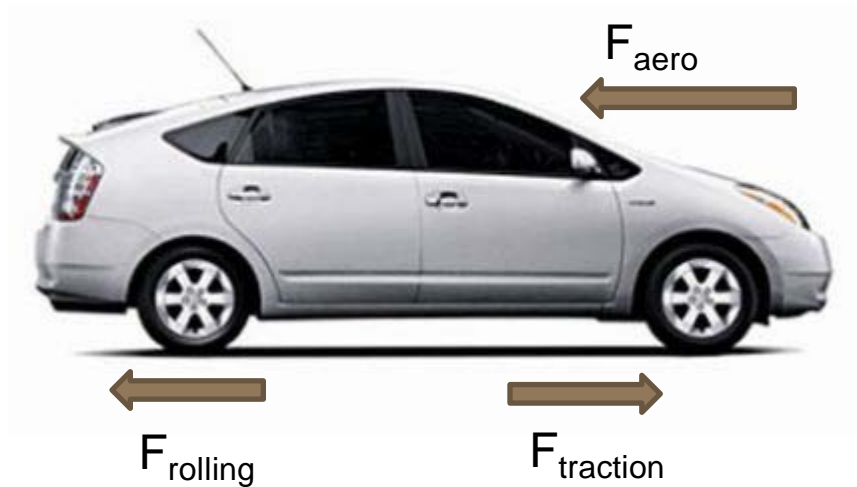
Three standard drive cycles are used for the comparison of two traction motors: a permanent magnet motor and a copper rotor induction motor. The 120,000/10year vehicle life is assumed to be composed equally of these three types of driving



| | Driving cycle | Distance | Average speed |
|---|-------------------|------------|---------------|
| — | City (UDDS) | 7.5 miles | 20 mph |
| — | Highway (HWFET) | 10.3 miles | 48 mph |
| — | Aggressive (US06) | 8.0 miles | 48 mph |

2. Vehicle Model

A standard vehicle model is used to convert drive cycle information into powertrain torque/speed requirements.



$$F_{rolling} = k_r mg$$

$$F_{aero} = \frac{1}{2} \rho v^2 C_d A_f$$

$$T_{motor} = k_{dem} \frac{F_{traction} \cdot r_{\omega}}{n_d}$$

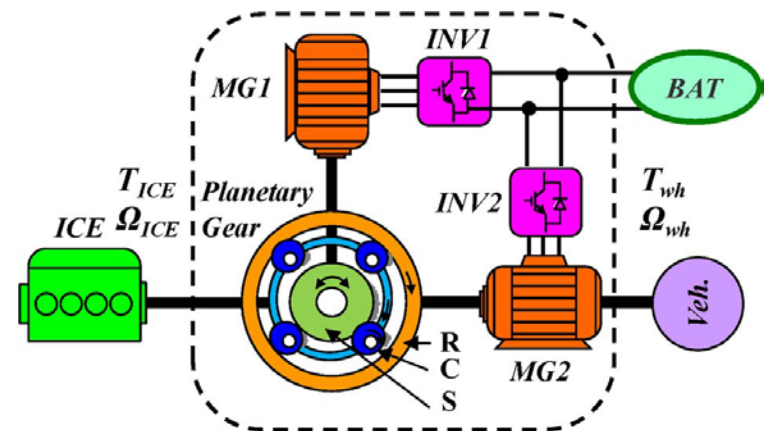
$$Acceleration\ of\ Vehicle = \frac{(F_{traction} - F_{aero} - F_{rolling})}{m}$$

3.1 Powertrain model

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A standard two motor/generator hybrid powertrain architecture is used

- Consists of two electrical motor/generators, MG1 and MG2 and an internal combustion engine, all connected through a planetary gear set
- Rotational speed of the internal combustion engine (ICE) is decoupled from the vehicle speed to maximise efficiency
- We analyze MG2 for performance/cost
- We assume that MG2:
 - Has a rated power of 50kW
 - Couples to the drive wheels through a fixed gear ratio
 - Provides 30% of motoring torque
 - Recovers up to 250Nm braking torque
 - The ICE and brakes supply the rest

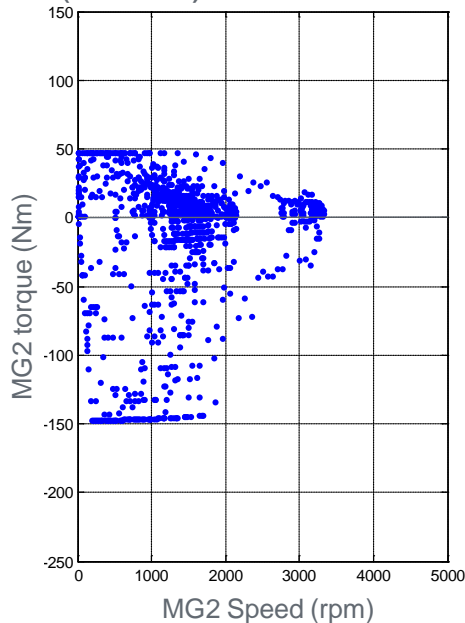


3.2 Motor torques/speeds produced during driving cycles

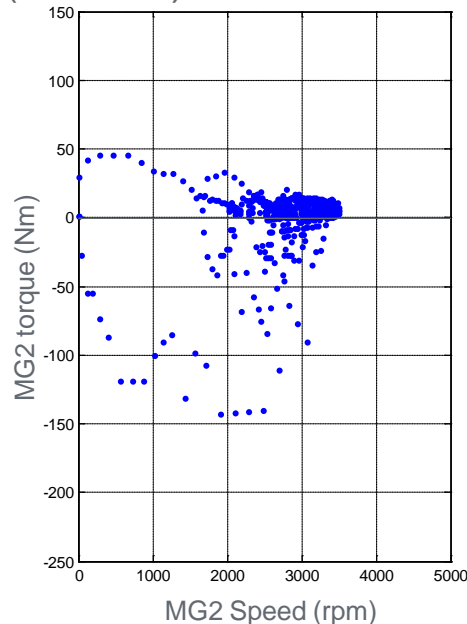
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By applying the vehicle and powertrain models we convert the driving cycle data into motor torque/speed data points. One data point is produced for each one second of driving cycle

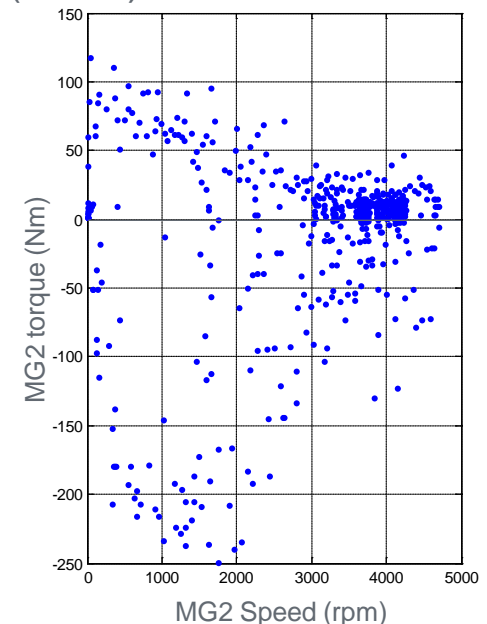
City cycle MG2 loads (UDDS)



Highway cycle MG2 loads (HWFET)



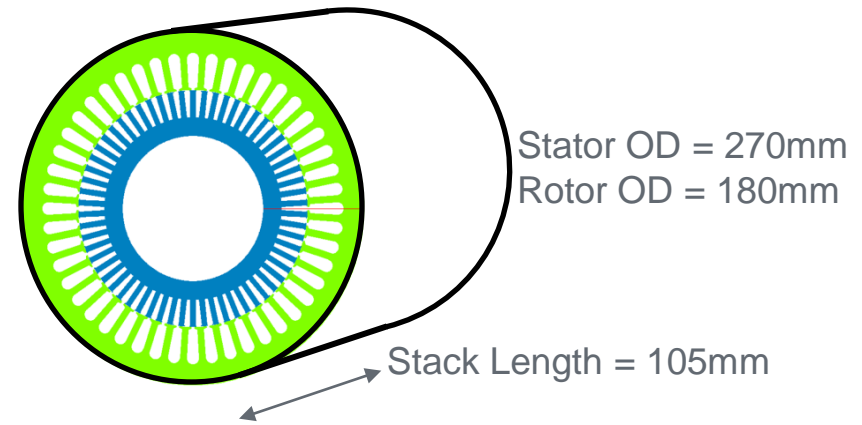
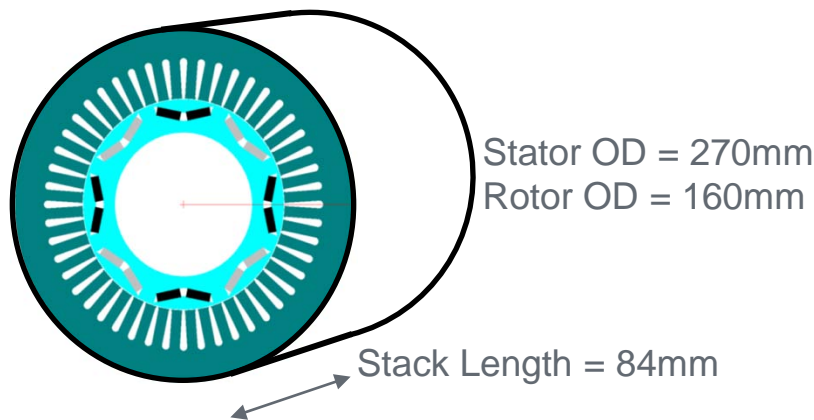
Aggressive cycle MG2 loads (US06)



4.1 Magnetic models of permanent magnet motor and induction motor

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The two motor types were modeled for similar torque/speed performance: same stator outside diameters, same cooling requirements but different stack lengths

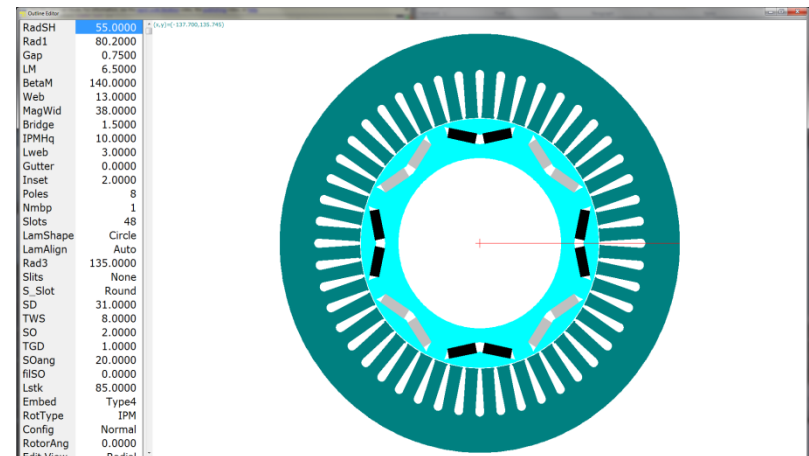
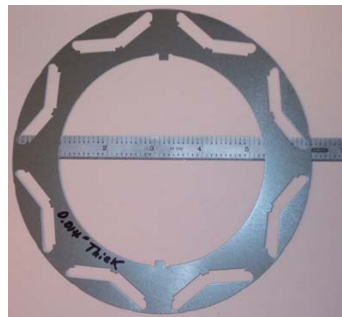
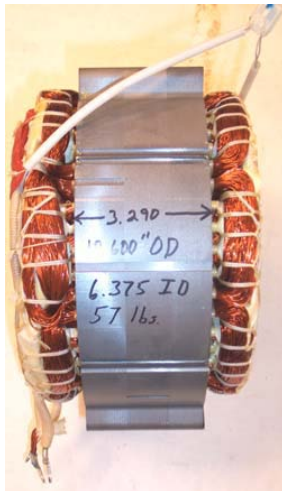


| Permanent Magnet Motor | | Copper Rotor Induction Motor |
|------------------------|--------------|------------------------------|
| 8 | Poles | 8 |
| 48 | Stator Slots | 48 |
| - | Rotor Bars | 62 |

4.2 Reference permanent magnet motor model

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The modelled permanent magnet motor is a well-documented actual motor used in a production hybrid vehicle.

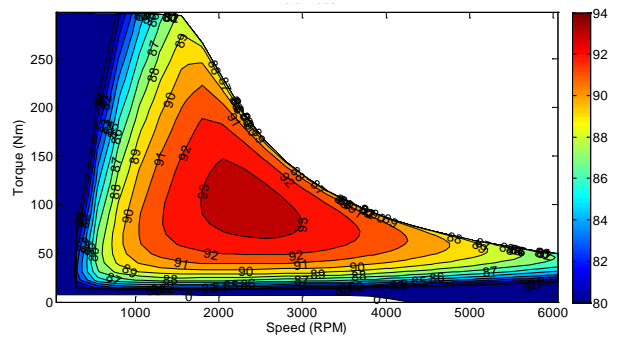


4.3 Validation of the motor performance model

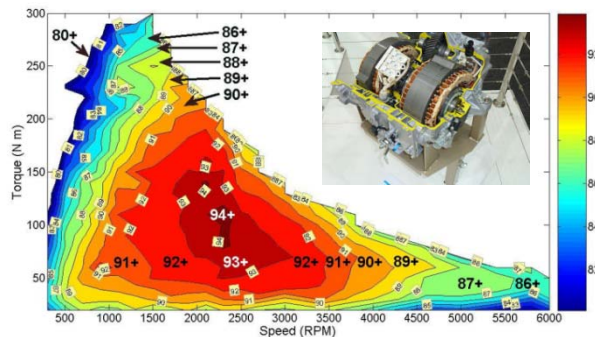
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The model of the permanent magnet motor was validated against test data from the actual motor

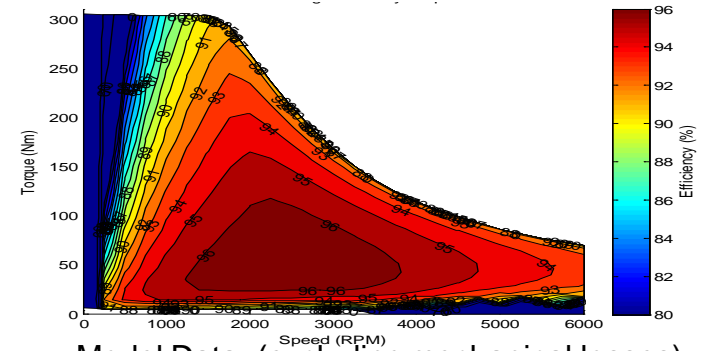
Model and actual data correspond well



Model data (including mechanical losses)



Test data from actual motor (including mechanical losses)

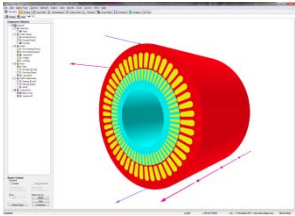


Model Data (excluding mechanical losses)

Our analysis continues using motor performance which excludes mechanical losses

4.4 Thermal Performance Comparison

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Steady-state thermal analysis was used to equalize cooling system requirements for both motors at a 118 Nm/900 rpm operating point

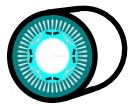


| Permanent Magnet Motor | | Copper Rotor Induction Motor |
|------------------------|----------------------|------------------------------|
| 92% | Efficiency | 88% |
| 780 W | Stator Copper Loss | 940 W |
| 0 W | Rotor Loss | 230 W |
| 0 W | Stray Load Loss | 140 W |
| 100 W | Iron Loss | 180 W |
| 880 W | Total Loss | 1490 W |
| 105°C | Coolant Temperature | 105°C |
| 2.4 gallons/min | Coolant Flow Rate | 2.4 gallons/min |
| 156°C | Maximum Winding Temp | 156°C |

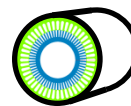
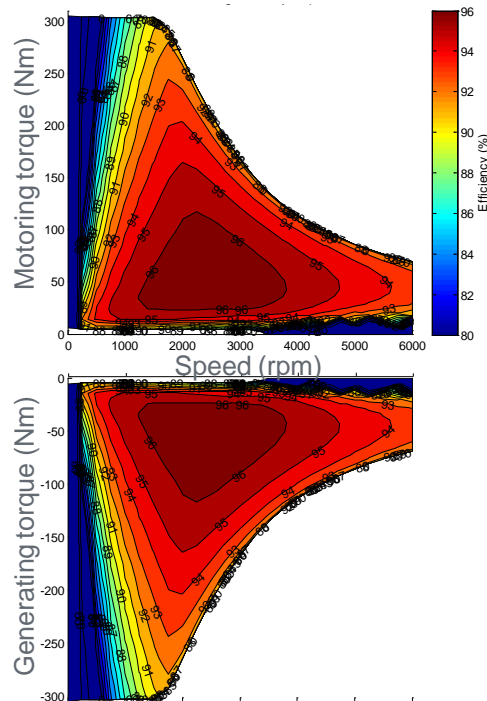
5.1 Torque/speed/efficiency maps of the permanent magnet motor and induction motor

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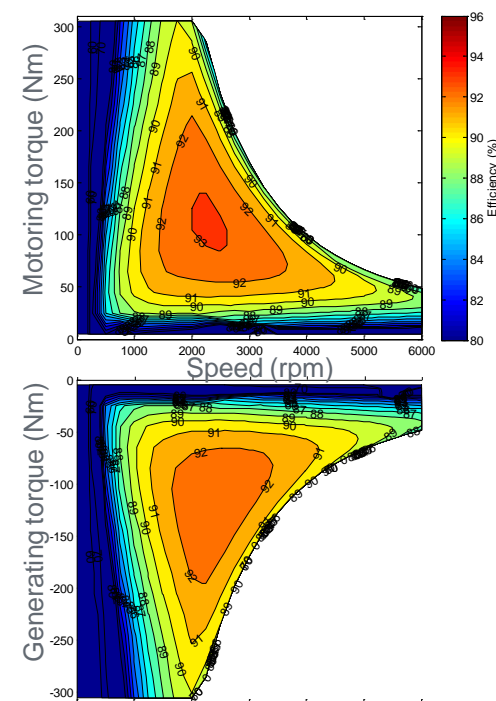
The two motors have similar torque/speed performance, with the induction motor having ~5% lower efficiencies



Permanent magnet motor



Copper rotor induction motor

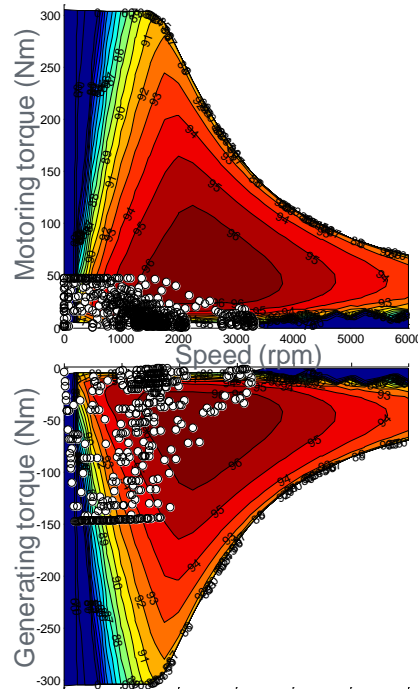


5.2 Torque/speed loads during drive cycles: permanent magnet motor

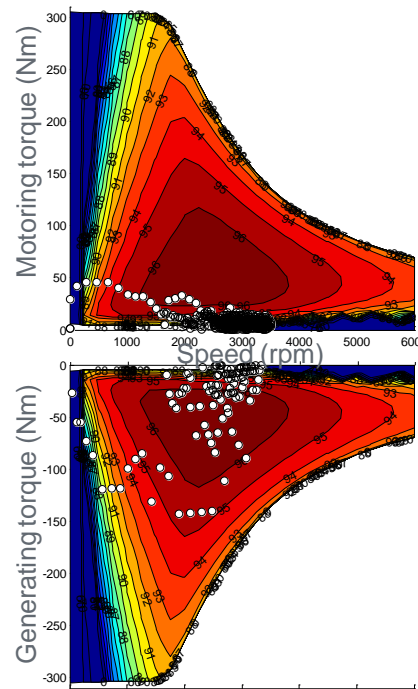
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Torque/speed points from the vehicle/powertrain model of the driving cycles are applied to the performance map of the permanent magnet motor to determine total motor losses during driving:

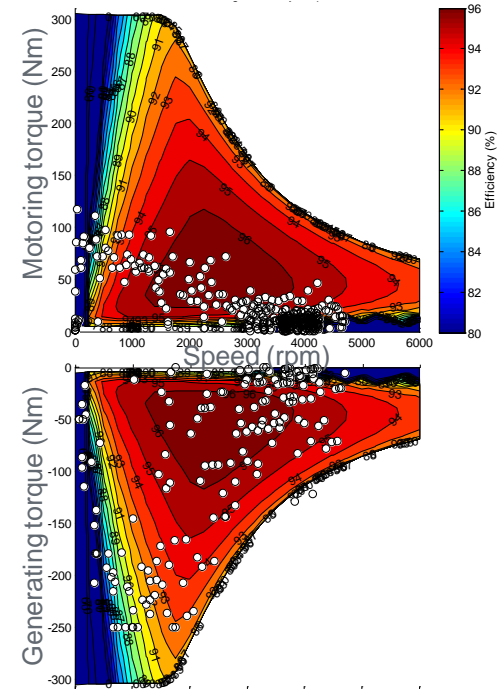
City driving cycle loads (UDDS)



Highway driving cycle loads (HWFET)



Aggressive driving cycle loads (US06)



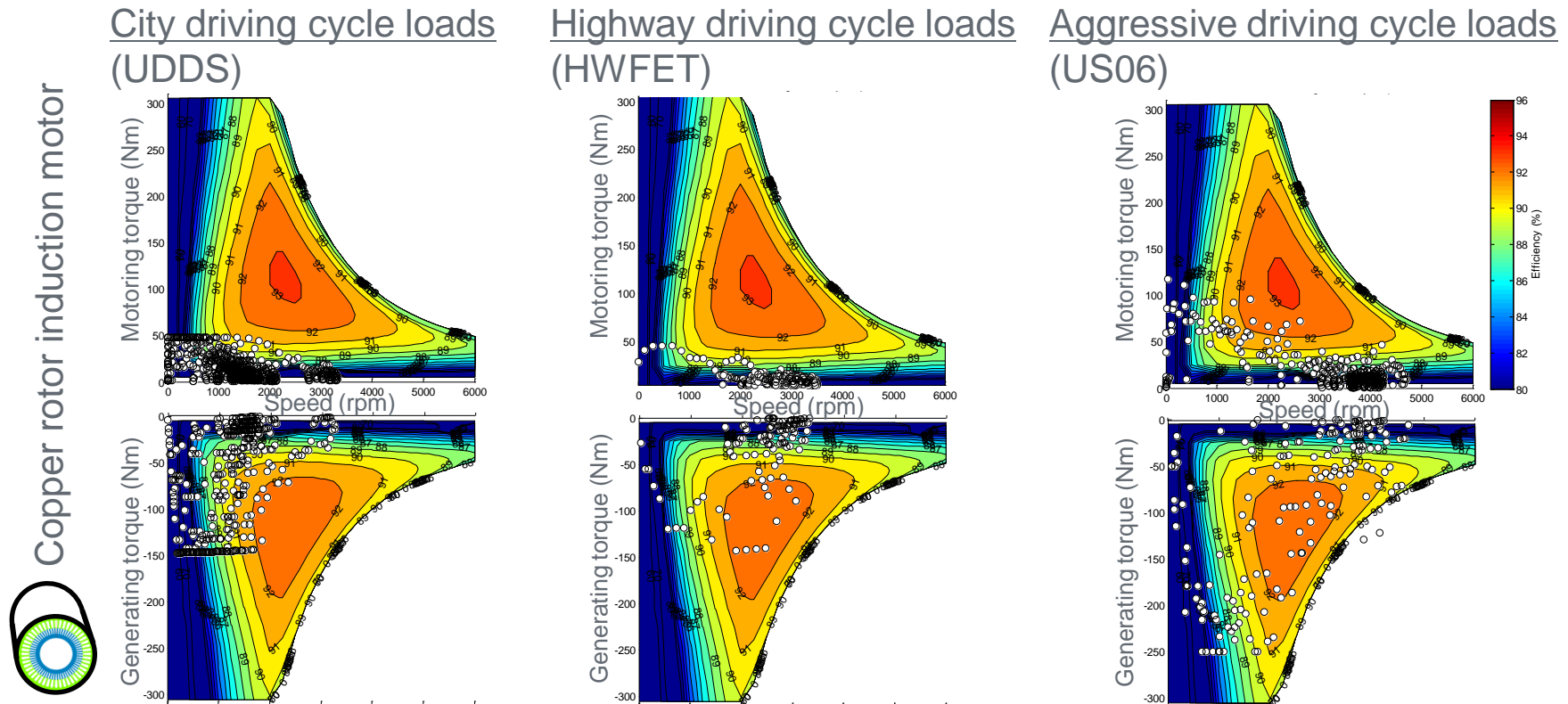
Permanent magnet motor



5.3 Torque/speed loads during drive cycles: copper rotor induction motor

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Torque/speed points from the vehicle/powertrain model of the driving cycles are applied to the performance map of the copper rotor induction motor to determine total motor losses during driving:

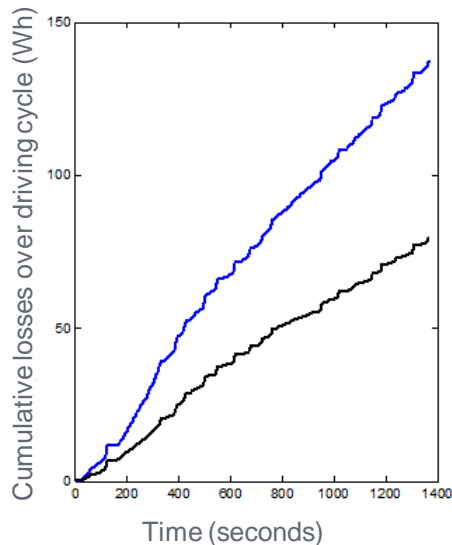


6.1 Motor losses during driving cycles

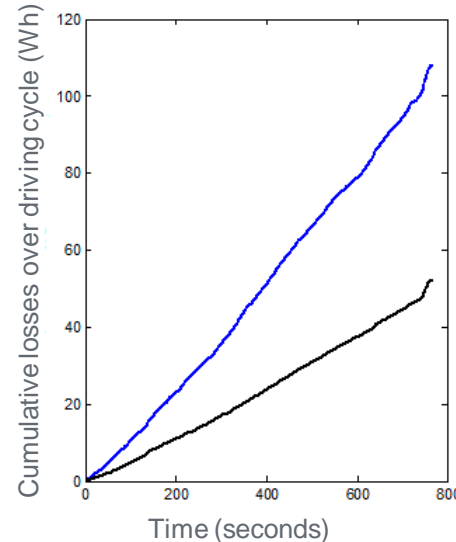
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From the motor models, cumulative losses during each driving cycle can be calculated:

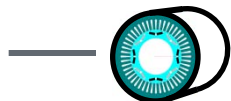
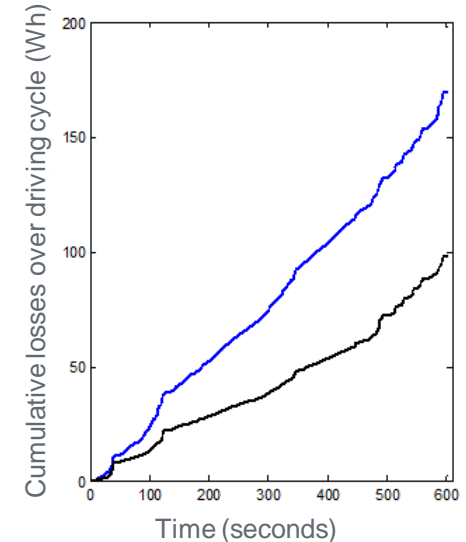
City driving cycle losses (UDDS)



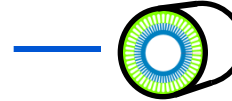
Highway driving cycle losses (HWFET)



Aggressive driving cycle losses (US06)



Permanent magnet motor

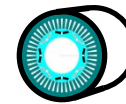


Copper rotor induction motor

6.2 Combined losses over life of the motor

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The total difference in electrical running costs between the permanent magnet motor and the copper rotor induction motor are \$220-\$260. Over a typical lifetime of 120,000 miles and 10 years, this is an insignificant cost.

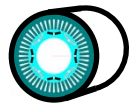


| Total losses in the motor | Permanent magnet motor | Copper rotor induction motor |
|--|------------------------|------------------------------|
| City driving over 120,000 miles (UDDS) | 1270 kWh | 2240 kWh |
| Highway driving over 120,000 miles (HWFET) | 610 kWh | 1250 kWh |
| Aggressive driving over 120,000 miles (US06) | 1430 kWh | 2510 kWh |
| Combined average losses over 120,000 miles | 1100 kWh | 2000 kWh |
| Extra energy cost (grid price of \$0.25/kWh) | 0 | \$220 |
| Extra energy cost (internal combustion engine cost of \$0.294/kWh) | 0 | \$260 |

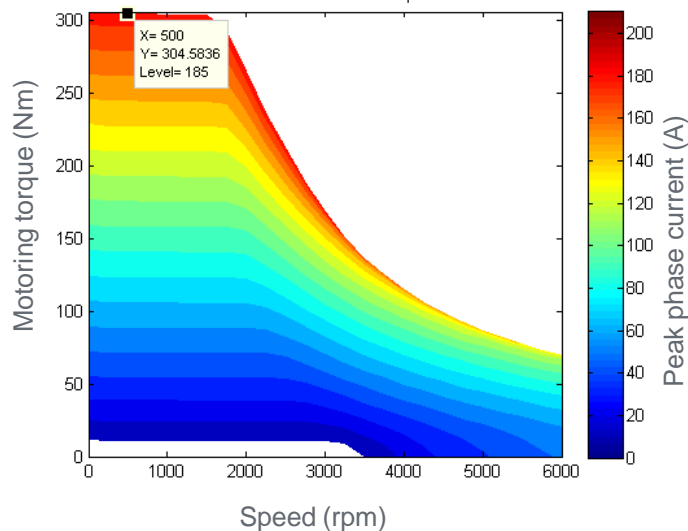
7. Cost of increased inverter for copper motor induction motor

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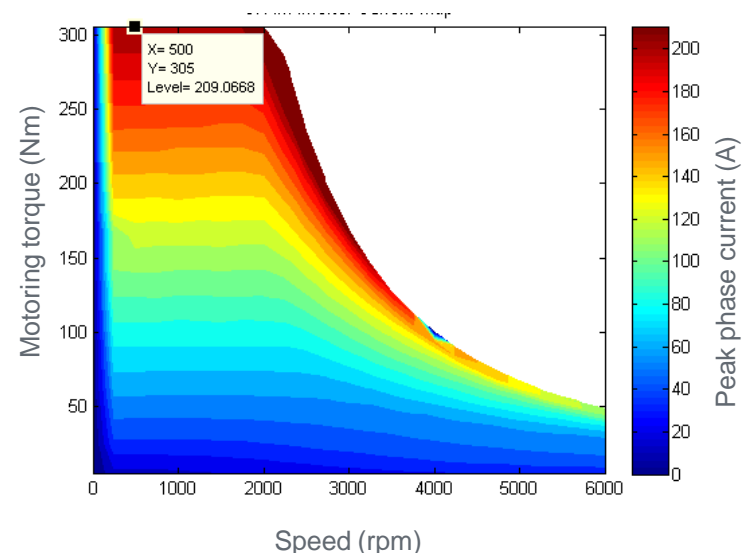
The copper rotor induction motor/generator requires 10-15% more current to achieve maximum torque. This requires that the power electronics cost ~\$50 more than for a permanent magnet motor.



Permanent magnet motor



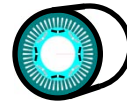
Copper rotor induction motor



8. Component cost comparison

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The copper rotor induction motor saves between \$60 (at 2013 magnet prices) and \$390 (at 2011 magnet prices) costs per vehicle. This translates into \$150-980 purchase price savings for the consumer



| Materials per motor | Permanent magnet motor | | Copper rotor induction motor | |
|---------------------------------------|------------------------|------------------|------------------------------|------------------|
| | Weight | Cost | Weight | Cost |
| Stator Copper | 4.5 kg | \$31 | 9.1 kg | \$64 |
| Steel | 24 kg | \$24 | 24 kg | \$24 |
| Permanent magnets (2011/2013 prices) | 1.3 kg | \$200-540 | 0 | 0 |
| Rotor cage | 0 | 0 | 8.4 kg | \$59 |
| Increased inverter cost | - | 0 | - | \$50 |
| Total | 29.8 kg (100%) | \$260-590 | 41.5 kg (140%) | \$200 |
| Reduction in consumer purchase price* | - | 0 | - | \$150-980 |

* Assumes materials-cost/consumer-price ratio = 40%

9. Cost of increased battery capacity to cover increased motor losses

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Using a copper rotor induction motor can require the vehicle designer to increase the battery size by ~7%. This would allow a customer to perceive no difference in overall vehicle performance.

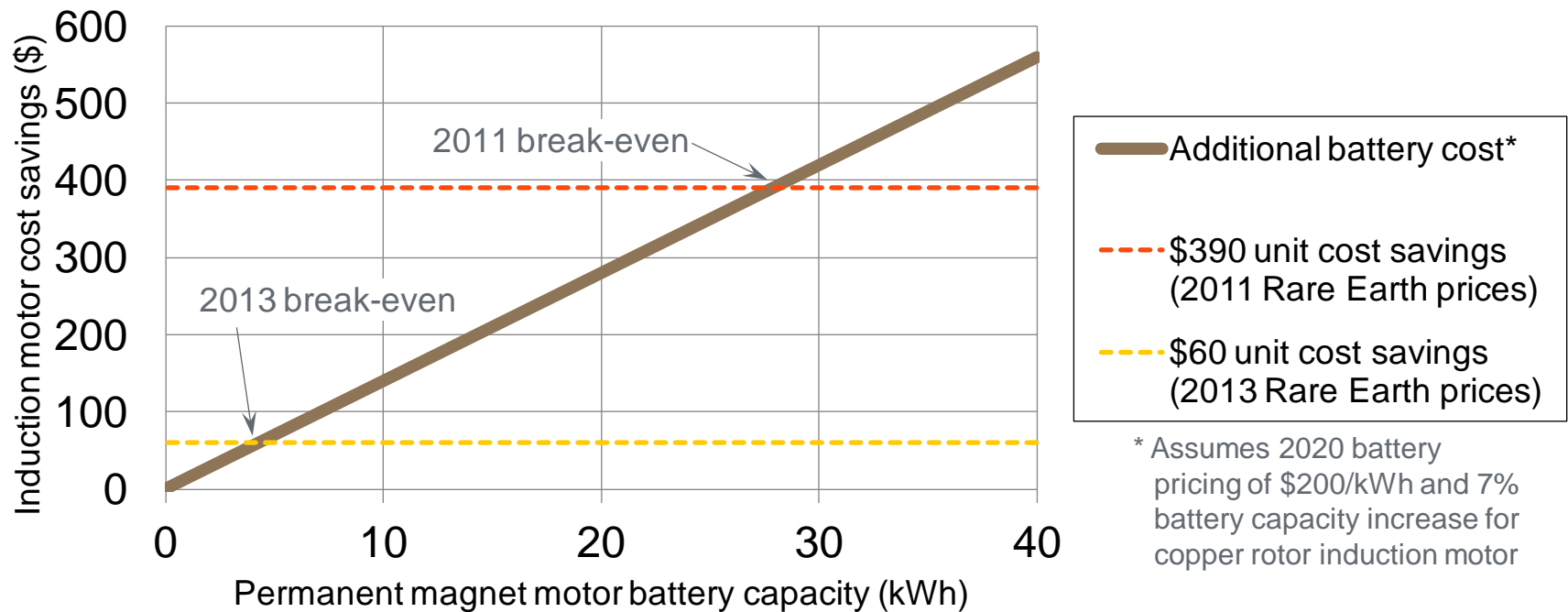
Key assumptions used in costing the required increase in battery capacity:

- Motor must at some time provide all motoring and braking torque in the highway driving cycle (like a plug-in hybrid electric vehicle)
- Induction motor uses 7% more motoring energy than a permanent magnet motor
- Induction motor recovers 6% less braking energy than the permanent magnet motor
- Total braking energy is 20% of the motoring energy over the driving cycle
- 75% of battery energy is used for motoring, 25% for auxiliary systems (cabin conditioning, lights, radio, electronics)

10. Break-even for using copper motor induction motor

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If the designer chooses to increase battery size for a 50kW system, a copper rotor induction motor saves total vehicle costs when the battery size for a permanent magnet motor system is less than 27kWh



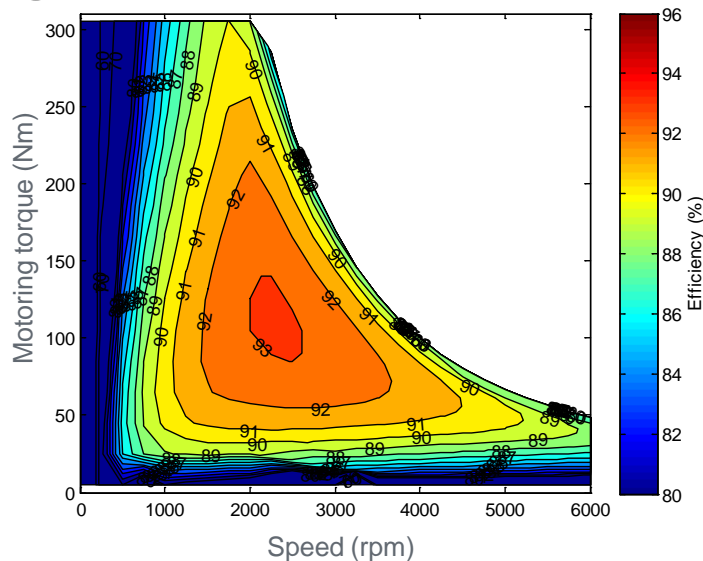
Possible use of aluminum in the rotor of an induction motor

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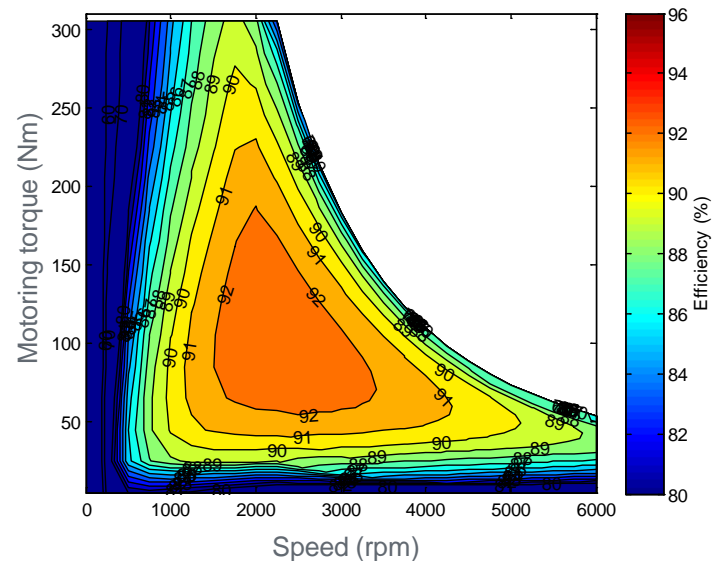
Aluminum has only 56% of the conductivity of copper, which leads to an inferior performance when used in the rotor of an induction motor. In a first-pass analysis of a 50kW aluminum rotor induction motor, losses were 4% higher and power/torque densities 5% lower than the equivalent copper rotor motor.



Copper rotor induction motor



Aluminum rotor induction motor



Main conclusions from this work

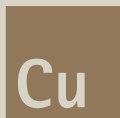
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Thank you

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